

EXPERIMENTAL AND NUMERICAL INVESTIGATION OF CEMENT PASTE MICROSTRUCTURE AND ITS HYDRATION UNDER SHORT-TERM EXPOSURE TO ACETONE

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ABSTRACT. The solvent exchange methods are commonly used in order to arrest cement hydration reaction. This paper presents preliminary results of experimental investigation of cement paste microstructure under short-term (24 hours) exposure to acetone as a solvent in order to estimate the influence of solvent soaking time. The methodology to determine the effect of soaking time based on numerical prediction is also presented and described. The immersion of cement samples with the cross-section of 10×10 mm in acetone for 24 hours at the sample age of 15 hours does not enable to fully stop the hydration reaction, however, it can slow down the hydration reaction significantly. According to the comparison of several measured data (nanoindentation, scanning electron microscopy, observation made by optical microscope, mercury intrusion porosimetry) at the sample age of 1 month with the numerical simulation, the equivalent sample age is determined as approximately equal to 69 hours.

KEYWORDS: Acetone, cement paste, experiment, hydration reaction, numerical simulation.

1. INTRODUCTION

The hydration process of cement paste often has to be stopped in order to allow precise investigation and measurements of the alteration of cement paste properties over time. There are a numerous amount of methods to stop the hydration reaction [1–4], which can be divided into the following two groups:

- (1.) Direct drying. The essence of the direct drying methods is to transform water into the vapor. The water vapor may escape freely and hydration reaction stops due to the lack of water, however, the direct drying methods are accompanied by the rapid change in temperature or pressure, which may damage microstructure of the sample or alter the cement paste properties and distort the results of the measurements [5–7]. The following types of direct drying are used in the available literature:
 - oven drying [5, 8, 9],
 - microwave drying [10–12],
 - vacuum drying [13],
 - freeze drying [14],
 - D-drying [15],
 - P-drying [15], etc.
- (2.) Solvent exchange. The mechanism of solvent exchange methods is following: the solvent penetrates into the sample, mixes with free water and evaporates rapidly due to its low boiling point. It is believed that solvent exchange methods have lower impact on cement paste microstructure, however, it

was reported [16, 17] that solvents may react with cement paste hydrates and alter its properties. Also, it is difficult to entirely remove solvents, therefore, the chemical composition of the cement paste may be affected by the solvent. The following types of solvents are used in the available literature:

- acetone [8, 18],
- methanol [19, 20],
- ethanol [21, 22],
- isopropanol [14, 19],
- tetrahydrofuran [1],
- dimethyl sulfoxid [20],
- benzene [16],
- pentane [23], etc.

From the above, it is obvious that the method to stop the hydration reaction should be chosen according to the subject of interest. This study is focused on cement paste microstructure investigation, therefore, the solvent exchange method was chosen and the acetone was used as the solvent.

The necessary solvent soaking time to stop the hydration reaction depends on many factors, such as porosity, diffusivity, sample cross-section. Porosity and diffusivity of early age cement paste change rapidly over time, therefore, the necessary solvent soaking time has to be a function of cement paste age. The majority of the research does not provide a sufficient explanation of the chosen soaking time.

Another complication is that it is impossible to determine whether the reaction was stopped during the solvent soaking and the additional experiments are needed for this purpose. Therefore, the experimental investigation of the influence of solvents on cement paste has to be performed in order to determine the necessary solvent soaking time to stop the hydration reaction of early-age cement paste.

This paper presents preliminary results of the experimental investigation of early-age cement paste microstructure change under short-term (24 hours) exposure to acetone in order to estimate the influence of acetone soaking time. The methodology to determine the effect of soaking time based on the numerical prediction is also presented and described in detail below.

2. EXPERIMENT

The cement paste which consists of CEM I 42.5R EXTRACEM and water with water-to-cement ratio of 0.38 was used to produce small-scale 10x10x80 mm samples. The cement clinker composition is shown in Table 1. The samples together with the plexiglass moulds were insulated by polyethylene foil till the age of 15 hours.

After demoulding, all the samples were immersed in acetone for 24 hours at the sample age of 15 hours in order to stop the hydration process. After that all the samples were dried in oven at 50 °C till equilibrium in order to remove acetone. The samples were packed in polyethylene foil and were stored in box with silica gel until the examination in order to avoid possible moisture ingress [24].

Environmental temperature and relative humidity were recorded starting from the mixing till packing with the interval of 1 minute. The average environmental temperature was 20.7 °C and relative humidity was 72.8% (excluding oven drying).

The amount of anhydrous clinker was obtained using three different techniques, namely, nanoindentation (NANO), scanning electron microscopy (SEM) and observation made by optical microscope (OPT) at the sample age of one month.

The surface of the sample sections, which were used for nanoindentation and SEM and OPT investigation, was polished with silica carbide paper to achieve a smooth surface. The nanoindentation of the polished sample sections was carried out with a Hysitron TriboLab Ti-700 with the Berkovich diamond tip. Five grids of 10 x 10 indents with the spacing of 10 µm were predetermined on the center part of the sample surface. The nanoindentation was performed using the force control test with the trapezoidal loading diagram. The sample surface was loaded by the diamond tip linearly during three seconds till the maximum force of 2 mN was reached with a following 20 seconds holding period and 3 seconds of unloading. The indentation elastic modulus was determined from the obtained load-displacement curves using the Oliver

and Pharr theory [25]. The values of the elastic modulus higher than 50 GPa and hardness higher than 1.5 GPa correspond to the anhydrous clinker.

After the nanoindentation, the polished sample sections were dried in a vacuum for three hours with a vacuum pump. The microstructure investigation of these sample sections was carried out by a Phenom XL Desktop SEM and optical microscope. The amount of anhydrous clinker was obtained using the image processing technique which was performed by the FIJI code. The measured volume fractions of anhydrous clinker and the average value are shown in Table 2.

The sample porosity and its distribution was measured using mercury intrusion porosimetry (MIP) at the sample age of one month. The sample sections were broken into pieces and the center pieces were selected for further porosity investigation by the mercury porosimeter PASCAL 140 a 440. The measured porosity was in the range from 32.6% to 36.7% for different samples.

More detailed description of the experiment is given in [24].

3. NUMERICAL SIMULATION

In order to understand whether the hydration reaction was fully stopped after the samples immersion in acetone, the MATLAB code of hydration and microstructure models, which is based on the models described in [26–28], was developed. The data presented in Table 1 and the measured environmental conditions were used in the analysis. The preliminary results are described below.

The degree of hydration was calculated using the multi-component model, where the rate of cement hydration heat generation is obtained from the sum of the hydration heat rates of cement components according to their proportions in cement. The degree of hydration was calculated according the following formula

$$\alpha_{hyd} = \sum p_i \cdot (\bar{Q}_i / \bar{Q}_{i,\infty}), \quad (1)$$

where p_i is the mass ratio of the chemical component i of cement (C2S, C3S, C3A, C4AF, gypsum, etc.), \bar{Q}_i is the accumulated heat generation of the chemical component i , $\bar{Q}_{i,\infty}$ is the maximum theoretical specific heat of the component i and α_{hyd} is the averaged degree of hydration.

The calculated degree of hydration of the individual clinker components and their average and time when the samples were immersed in acetone are shown in Figure 1 [24].

The cement paste microstructure was modeled using the expanding cluster model, volumetric balance and simplified calculation of the total pore surface area described in detail in [26–28]. After that the pore size distribution was calculated using a simplistic Raleigh-Ritz distribution function.

C3S, [%]	C2S, [%]	C3A, [%]	C4AF, [%]
63.99	14.30	9.11	8.26

C3S: Alite; C2S: Belite; C3A: Celite; C4AF: Felite.

TABLE 1. Clinker composition of CEM I 42.5R EXTRACEM according to the manufacturer [24].

NANO, [%]	SEM, [%]	OPT, [%]	Average, [%]
18.40	18.30	18.89	18.53

TABLE 2. Volume fractions of anhydrous clinker.

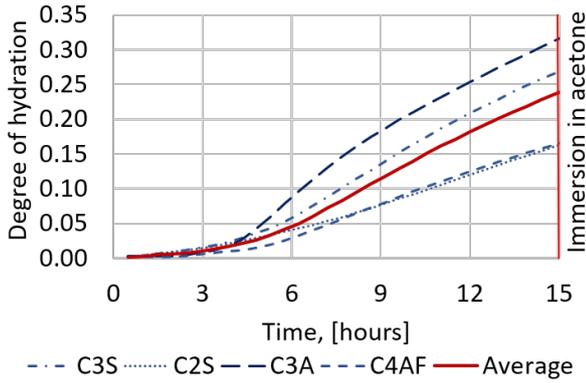


FIGURE 1. Calculated degree of hydration [24].

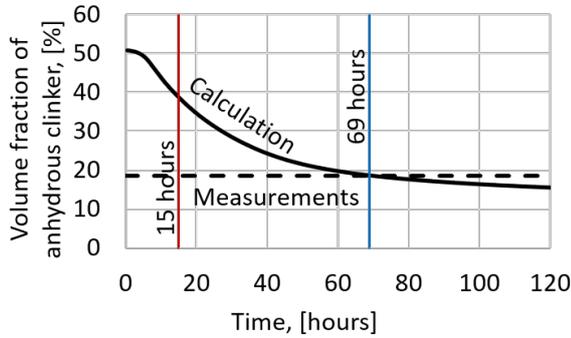


FIGURE 2. Amount of anhydrous clinker.

The volume fraction of anhydrous clinker was calculated as follows

$$V_{cl} = (1 - \alpha_{hyd}) \cdot W_p / \rho_p, \quad (2)$$

where W_p is the weight of powder materials per unit paste volume, ρ_p is the density of powder materials and V_{cl} is the volume fraction of anhydrous clinker.

The decrease of the amount of anhydrous clinker due to the hydration reaction over time with the depiction of the averaged measured value is shown in Figure 2 [24].

The capillary porosity was calculated using the following equation

$$\phi_c = 1 - V_s - V_{cl}, \quad (3)$$

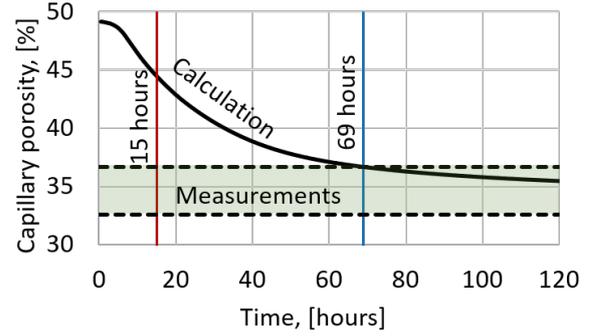


FIGURE 3. Capillary porosity.

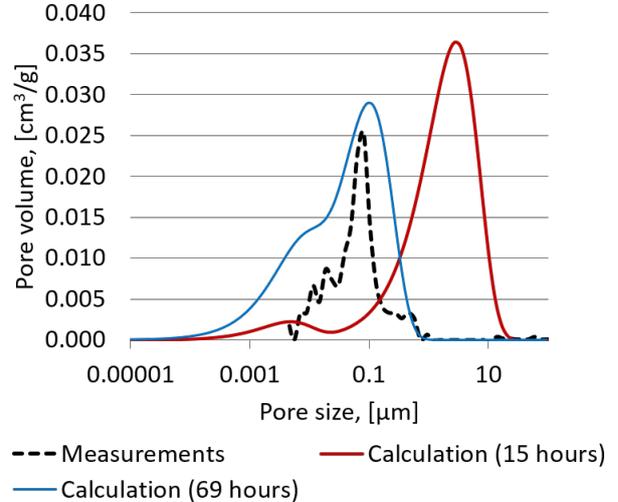


FIGURE 4. Pore size distribution.

where V_s is the volume of hydrated products and V_{cl} is the volume fraction of anhydrous clinker.

The pore size distribution was calculated as follows

$$\phi(r) = \phi_l + \phi_g \cdot V_g + \phi_c \cdot V_c, \quad (4)$$

where ϕ_l , ϕ_g and ϕ_c is the interlayer porosity, the gel porosity and the capillary porosity, respectively, $V_i = 1 - \exp(-B_i r)$ is the normalized pore volume, B_i is the porosity distribution parameter and r is the pore radius.

The calculated capillary porosity over time with the depiction of measured porosity (the total porosity

obtained using MIP is considered to be predominantly capillary porosity) is shown in Figure 3, while the measured and calculated pore distribution are shown in Figure 4 [24].

As can be seen in Figure 2, Figure 3 and Figure 4, the hydration reaction was not fully stopped at the sample age of 15 hours after sample immersion in acetone for 24 hours, but was slowed down significantly and the equivalent sample age is approximately equal to 69 hours according to the preliminary results of the numerical simulation at the real sample age of 1 month [24]. However, more detailed examination of the sample microstructure is still needed.

4. CONCLUSIONS

The immersion of cement samples with the cross-section of 10 x 10 mm in acetone for 24 hours at the sample age of 15 hours could not fully stop the hydration reaction, however, it can slow down the hydration reaction significantly. According to the comparison of the measured data at the sample age of 1 month with the numerical simulation, the equivalent sample age is approximately equal to 69 hours. The calculated volume fraction of anhydrous clinker, capillary porosity and pore size distribution have a good correlation with the measured values. However, the additional experiments with the variable acetone soaking time and different sample cross-section are necessary in order to draw the final conclusions.

LIST OF SYMBOLS

α_{hyd}	Averaged degree of hydration [-]
ρ_p	Density of powder materials [kg m^{-3}]
ϕ_c	Capillary porosity [-]
ϕ_g	Gel porosity [-]
ϕ_l	Interlayer porosity [-]
B_i	Porosity distribution parameter [-]
\overline{Q}_i	Accumulated heat generation of chemical component (C3S, C2S, C3A, C4AF) [kcal]
$\overline{Q}_{i,\infty}$	Maximum theoretical specific heat of component (C3S, C2S, C3A, C4AF) [kcal]
V_{cl}	Volume of anhydrous clinker [$\text{m}^3 \text{m}^{-3}$]
V_s	Volume of hydrated products [$\text{m}^3 \text{m}^{-3}$]
V_i	Normalized pore volume [$\text{m}^3 \text{m}^{-3}$]
W_p	Weight of powder materials per unit paste volume [kg m^{-3}]
p_i	Mass ratio of chemical component of cement (C3S, C2S, C3A, C4AF) [-]
r	Pore radius [m]

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