

FICTITIOUS DOMAIN METHOD FOR NUMERICAL SIMULATION OF INCOMPRESSIBLE VISCOUS FLOW AROUND RIGID BODIES

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ABSTRACT. This article describes the method of efficient simulation of the flow around potentially many rigid obstacles. The finite element implementation is based on the incompressible Navier-Stokes equations using structured, regular, two dimensional triangular mesh. The fictitious domain method is introduced to account for the presence of rigid particles, representing obstacles to the flow. To enforce rigid body constraints in parts corresponding to rigid obstacles, Lagrange multipliers are used. For time discretization, an operator splitting technique is used. The model is validated using 2D channel flow simulations with circular obstacles. Different possibilities of enforcing rigid body constraints are compared to the fully resolved simulations and optimal strategy is recommended.

KEYWORDS: finite element method; computational fluid dynamics; fictitious domain method; Lagrange multipliers; flow around obstacles.

1. INTRODUCTION

The motivation of the paper comes from the modeling of the fresh concrete casting. The simulation models of fresh concrete aiming at structural-scale applications typically consider concrete suspension as a homogeneous, non-Newtonian fluid, whose rheological properties can be derived from the mix composition [1]. The flow can be then efficiently described by Navier-Stokes equations considering non-Newtonian fluid and solved using the Finite Element Method (FEM), for example. Of course, the efficiency of the homogeneous approach comes at the expense of the coarser description of the flow, where sub-scale phenomena can only be approximately accounted for by post-processing simulation results, e.g. to determine the distribution and orientation of reinforcing fibers [2], or by heuristic modification of constitutive parameters, e.g. to account for the effect of traditional reinforcement [3]. Especially the latter aspect is critical in the modeling of casting processes in highly-reinforced structures that represent the major field of application for self-compacting concrete.

The explicit representation of individual reinforcing bars in the FE model would lead to extremely fine computational meshes and will result in extremely high computational demands in terms of resources and time. This article aims at reducing these computational costs by avoiding the need of explicit representation of individual reinforcing bars by adopting an approach based on fictitious domain method to solve the problem of Newtonian incompressible flow with rigid body obstacles on regular, structured computational grid, where the individual reinforcing bars can be inserted arbitrarily and independently of the underlying mesh. The individual bars are accounted for by enforcing no-flow constraints in a volume occupied

by the bar using Lagrange multipliers. To solve the incompressible Navier-Stokes problem, a 2D Eulerian formulation of finite element method is developed, using the “Taylor-Hood” P2/P1 elements, which are quadratic in velocity and linear in pressure, satisfying the LBB condition [4]. The time discretization is based on operator splitting approach, in particular, the fractional-time-step scheme described by Marchuk has been employed [5].

The fundamental idea of fictitious domain method consists in extending the problem to one geometrically simpler domain covering both fluid and obstacles – the so-called fictitious domain. The no-flow constraints in subdomains corresponding to individual bars are enforced using distributed Lagrange multipliers, which represent the additional body forces needed to enforce zero flow inside the regions representing obstacles. The pressure is constrained by incompressibility of the fluid in the fictitious domain. This so called distributed Lagrange multiplier fictitious domain method has been introduced by Glowinski et al. [6]. The method has then been used by Bertrand et al. [7] and Tanguy et al. [8] to calculate three-dimensional flows. Recently, the method has been extended by Baaijens [9] and Yu [10] to handle fluid-structure interactions.

The main advantage of this method is a much simpler generation of the computational grid, because the mesh does not need to conform to the geometry of the reinforcement. It can be fully structured and regular, allowing to take advantage of specialized, fast numerical solvers. This feature can significantly reduce computational requirements of the problem. To the authors knowledge, there has been no study published investigating the influence of the sampling point selection on the quality of the solution. The

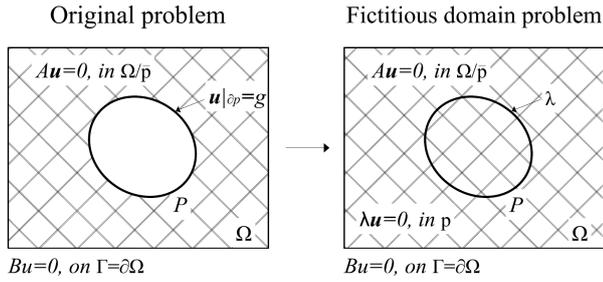


FIGURE 1. Original and fictitious domain problems.

goal of this paper is to propose and evaluate different strategies for enforcing no-flow constraints using different sets of sampling points and compare their performance to the fully resolved simulations.

1.1. FICTITIOUS DOMAIN METHOD

The basic idea of the method is based on a cancellation of the forces and moments between obstacles and fluid in the combined weak formulation for particle-fluid motion solved everywhere in the fictitious domain. To enforce the no-flow constraints (sometimes referred as rigid-body constraints when moving rigid particles are considered) to account for rigid particles, Lagrange multipliers are introduced. These multipliers represent the additional body forces needed to maintain the rigid body motion inside the moving particles or the no flow constraint inside the regions representing fixed particles. As already mentioned, the advantage of this approach consist in ability to use geometrically simpler, regular meshes.

2. PROBLEM FORMULATION

2.1. THE GOVERNING EQUATION OF THE FLOW

Assume an incompressible, viscous, Newtonian fluid occupying at the given time $t \in (0, T)$ the delimited domain $\Omega \subset \mathbf{R}^2$ with boundary Γ . Let denote by $\mathbf{x} = \{x_i\}_{i=1}^2$ a generic point in Ω . Let further denote by $\mathbf{u}(\mathbf{x}, t)$ velocity and by $p(\mathbf{x}, t)$ pressure, both governed by Navier-Stokes equations

$$\varrho \frac{d\mathbf{u}}{dt} = \varrho \mathbf{g} + \nabla \cdot \boldsymbol{\sigma} \quad \text{on } \Omega \setminus \bar{P}, \quad (1)$$

$$\nabla \cdot \mathbf{u} = 0 \quad \text{on } \Omega \setminus \bar{P}, \quad (2)$$

where ϱ is density of the fluid, \mathbf{u} is velocity of the fluid, and $\boldsymbol{\sigma}$ is stress tensor. For an incompressible, Newtonian viscous fluid, the stress can be decomposed into hydrostatic and deviatoric components

$$\boldsymbol{\sigma} = -p\mathbf{I} + 2\eta\mathbf{D}[\mathbf{u}], \quad (3)$$

where p is hydrostatic pressure in the fluid, η is the viscosity (assumed constant), and $2\eta\mathbf{D}[\mathbf{u}]$ is deviatoric stress tensor.

Relations (1)–(3) are to be complemented by the appropriate initial and boundary conditions

$$\mathbf{u}(\mathbf{x}, 0) = \mathbf{u}_0 \quad \text{on } \Omega \setminus \bar{P}, \quad (4)$$

$$\nabla \cdot \mathbf{u}_0 = 0, \quad (5)$$

$$\mathbf{u}(\mathbf{x}, t) = \mathbf{u}_\Gamma(t) \quad \text{on } \Gamma, \quad (6)$$

$$\int_\Gamma \mathbf{u}_\Gamma(t) \hat{\mathbf{n}} d\mathbf{x} = 0, \quad (7)$$

where $\hat{\mathbf{n}}$ is unit normal vector pointing out of Γ .

2.2. GOVERNING EQUATIONS FOR OBSTACLES

Hydrodynamic force \mathbf{F}_i and torque \mathbf{T}_i acting on the i -th particle can be evaluated by summing up corresponding fluid induced forces acting on the particle boundary:

$$\mathbf{F}_i = \int_{\partial P_i} \boldsymbol{\sigma} \hat{\mathbf{n}} ds, \quad \mathbf{T}_i = \int_{\partial P_i} \mathbf{r}_i x \boldsymbol{\sigma} \hat{\mathbf{n}} ds, \quad (8)$$

where P_i is the region occupied by the particle and $\mathbf{r}_i = \mathbf{x} - \mathbf{X}_i$ is relative position vector to particle center \mathbf{X}_i .

3. WEAK FORM

Let us introduce the approximation of spaces for test and trial functions for velocities and pressure in the fluid part of domain $\Omega \setminus \bar{P}$ without obstacles:

$$\begin{aligned} \mathbb{W} &= \{ \mathbf{u} \in H^1(\Omega \setminus \bar{P}) : \mathbf{u} = \mathbf{u}_\Gamma(t) \text{ on } \Gamma \}, \\ \mathbb{V} &= \{ \mathbf{v} \in H^1(\Omega \setminus \bar{P}) : \mathbf{v} = 0 \text{ on } \Gamma \}, \\ L &= \{ p \in L^2(\Omega \setminus \bar{P}) \}, \\ \mathbb{K} &= \{ q \in L^2(\Omega \setminus \bar{P}) \}. \end{aligned}$$

By using the method of weighted residuals applied to (1), (2) and using finite dimensional spaces $\mathbb{W}_{0,h}$, $\mathbb{V}_{0,h}$, $L_{0,h}$, $\mathbb{K}_{0,h}$, approximating \mathbb{W} , \mathbb{V} , L , \mathbb{K} defined above we arrive at the following finite-element approximation of the Navier-Stokes equations:

Find $\mathbf{u}_h \in \mathbb{W}_{0,h}$, $p \in L_{0,h}$ satisfying

$$\begin{aligned} \int_{\Omega \setminus \bar{P}} \left(\varrho \frac{\partial \mathbf{u}_h}{\partial t} + (\mathbf{u}_h \cdot \nabla) \mathbf{u}_h \right) \cdot \mathbf{v}_h d\mathbf{x} \\ - \int_{\Omega \setminus \bar{P}} p_h \nabla \cdot \mathbf{v}_h d\mathbf{x} + \int_{\Omega \setminus \bar{P}} 2\eta \mathbf{D}[\mathbf{u}_h] : \mathbf{D}[\mathbf{v}_h] d\mathbf{x} = 0 \end{aligned}$$

for all $\mathbf{v}_h \in \mathbb{W}_{0,h}$, (9)

$$\int_{\Omega \setminus \bar{P}} q_h \nabla \cdot \mathbf{u}_h d\mathbf{x} = 0 \quad \text{for all } q_h \in L_{0,h}, \quad (10)$$

$$\mathbf{u}_h(0) = \mathbf{u}_{0,h} \quad \text{on } \Omega, \quad (11)$$

where $\mathbf{u}_{0,h}$ is a divergence-free initial velocity.

Since in (9) \mathbf{u} is divergence-free and satisfies the Dirichlet boundary condition (4) on Γ , we can write

$$\int_{\Omega \setminus \bar{P}} 2\eta \mathbf{D}[\mathbf{u}_h] : \mathbf{D}[\mathbf{v}_h] d\mathbf{x} = \int_{\Omega \setminus \bar{P}} \eta \nabla \mathbf{u}_h : \nabla \mathbf{v}_h d\mathbf{x}$$

for all $\mathbf{v}_h \in \mathbb{W}_{0,h}$.

3.1. A FICTITIOUS DOMAIN FORMULATION

To extend from the domain $\Omega \setminus \bar{P}$ to the fictitious domain Ω , it is necessary to enforce no-flow constraints inside each P_i . Let us introduce an approximation of spaces for test and trial functions velocities and pressure for the fictitious domain Ω :

$$\begin{aligned}\mathbb{W} &= \{ \mathbf{u} \in H^1(\Omega) : \mathbf{u} = \mathbf{u}_\Gamma(t) \text{ on } \Gamma \}, \\ \mathbb{V} &= \{ \mathbf{v} \in H^1(\Omega) : \mathbf{v} = 0 \text{ on } \Gamma \}, \\ L &= \{ p \in L^2(\Omega) \}, \\ \mathbb{K} &= \{ q \in L^2(\Omega) \}.\end{aligned}$$

By extending the incompressibility condition to the whole Ω , we get

$$\int_{\Omega} q \nabla \cdot \mathbf{u} \, dx = 0 \quad \text{for all } q \in L_h^2(\Omega).$$

The condition to enforce rigid body (or no-flow) constraints for each obstacle can be expressed as

$$\mathbf{u}(\mathbf{x}, t) - \mathbf{u}(\mathbf{X}_i, t) = 0 \quad \text{for all } x \in \bar{P}. \quad (12)$$

To relax the no-flow constraint defined above, the family of Lagrange multipliers λ_j is introduced representing a discrete set of points covering P_j , such that

$$\Lambda_h = \left\{ \boldsymbol{\mu}_h : \boldsymbol{\mu}_h = \sum_{i=1}^M \boldsymbol{\mu}_i \delta(\mathbf{x} - \mathbf{x}_i), \boldsymbol{\mu}_1, \dots, \boldsymbol{\mu}_m \in R^2 \right\},$$

where δ is the Dirac delta function at $x = 0$. Using the space Λ_h defined above, the condition (12) is relaxed to

$$\langle \boldsymbol{\mu}_h, \mathbf{u}(\mathbf{x}, t) - \mathbf{u}(\mathbf{X}_i, t) \rangle = 0 \quad \text{for all } \boldsymbol{\mu}_h \in \Lambda_h, \quad (13)$$

where the inner product on the obstacle is defined as

$$\langle \boldsymbol{\mu}_h, \mathbf{v}_h \rangle_P = \sum_{i=1}^M \boldsymbol{\mu}_{h,i} \cdot \mathbf{v}_h(\mathbf{x}_i).$$

In case of a fixed particle, it is necessary to prescribe zero velocity at the particle center. In case of moving particle, the equations of motions for a particle have to be solved as well.

The combined weak solution is then to find $\mathbf{u}_h \in \mathbb{W}_{0,h}$, $p_h \in L_{0,h}$, where finite dimensional spaces $\mathbb{W}_{0,h}$, $L_{0,h}$ are approximating \mathbb{W} , L spaces defined above and $\boldsymbol{\lambda}_h \in \Lambda_h$ is such that

$$\begin{aligned}\int_{\Omega} \varrho \left(\frac{\partial \mathbf{u}}{\partial t} + (\mathbf{u}_h \cdot \nabla) \mathbf{u}_h \right) \mathbf{v}_h \, dx - \int_{\Omega} p_h \nabla \cdot \mathbf{v}_h \, dx \\ + \int_{\Omega} 2\eta \mathbf{D}[\mathbf{u}_h] : \mathbf{D}[\mathbf{v}_h] \, dx &= \langle \boldsymbol{\lambda}_h, \mathbf{v}_h \rangle_P \\ &\text{for all } \mathbf{v}_h \in \mathbb{V}_h, \\ \int_{\Omega} q_h \nabla \cdot \mathbf{u}_h \, dx &= 0 \quad \text{for all } q_h \in L_h^2, \\ \langle \boldsymbol{\mu}_h, \mathbf{u}_h \rangle_P &= 0 \quad \text{for all } \boldsymbol{\mu}_h \in \Lambda_h, \\ \mathbf{u}(0) &= \mathbf{u}_0 \quad \text{on } \Omega.\end{aligned}$$

3.2. TIME DISCRETIZATION BY OPERATOR SPLITTING

As pointed out by Glowinski [11], numerical solutions of the nonlinear partial differential Navier-Stokes equations are not trivial, mainly due to the following reasons: (i) the above equations are nonlinear and (ii) the incompressibility condition is difficult to handle. The above equations represent a system of partial differential equations, coupled through the nonlinear term, the incompressibility condition $\nabla \cdot \mathbf{u} = 0$, and sometimes through the boundary conditions.

The use of time discretization by operator splitting will partly overcome the above difficulties; in particular, decoupling of difficulties associated with the nonlinearity from those associated with the incompressibility condition. Following the work of Glowinski and Pironneau [12], assuming the following initial value problem

$$\begin{aligned}\frac{d\varphi}{dt} + A(\varphi) &= 0, \\ \varphi(0) &= \varphi_0,\end{aligned}$$

where A is an operator (possibly nonlinear, and even multivalued) from a Hilbert space H into itself and where $\varphi_0 \in H$. A number of splitting techniques have been proposed, for an overview, we refer to [5]. In this work, we have used the scheme proposed by Marchuk [5], which is described in the next section.

3.3. MARCHUK'S FRACTIONAL-STEP SCHEME

Marchuk assumed a decomposition of the operator A into the following nontrivial decomposition

$$A = A_1 + A_2 + A_3 \quad (14)$$

(by nontrivial, we mean that operators A_1 , A_2 and A_3 are individually simpler than A). By assuming a time discretization with the time step Δt , the updated value at the end of the time step can be computed using a three step integration procedure as follows:

$$\begin{aligned}\frac{\varphi^{n+1/3} - \varphi^n}{\Delta t} + A_1(\varphi^{n+1/3}) &= f_1^{n+1}, \\ \frac{\varphi^{n+2/3} - \varphi^{n+1/3}}{\Delta t} + A_2(\varphi^{n+2/3}) &= f_2^{n+1}, \\ \frac{\varphi^{n+1} - \varphi^{n+2/3}}{\Delta t} + A_3(\varphi^{n+1}) &= f_3^{n+1}.\end{aligned}$$

By applying an operator splitting to the problem (9)–(12), one obtains (with $0 \leq \alpha, \beta \leq 1$ and $\alpha + \beta = 1$):

Find $\mathbf{u}_h^{n+1/3} \in \mathbb{W}_h$ and $p^{n+1/3} \in L^h$ such that

$$\begin{aligned}\varrho \int_{\Omega} \frac{\mathbf{u}_h^{n+1/3} - \mathbf{u}_h^n}{\Delta t} \cdot \mathbf{v}_h \, dx - \int_{\Omega} p_h^{n+1/3} \nabla \cdot \mathbf{v}_h \, dx &= 0 \\ &\text{for all } \mathbf{v}_h \in \mathbb{V}_h, \quad (15) \\ \int_{\Omega} q_h \nabla \cdot \mathbf{u}_h^{n+1/3} \, dx &= 0 \quad \text{for all } q_h \in L_h^2. \quad (16)\end{aligned}$$

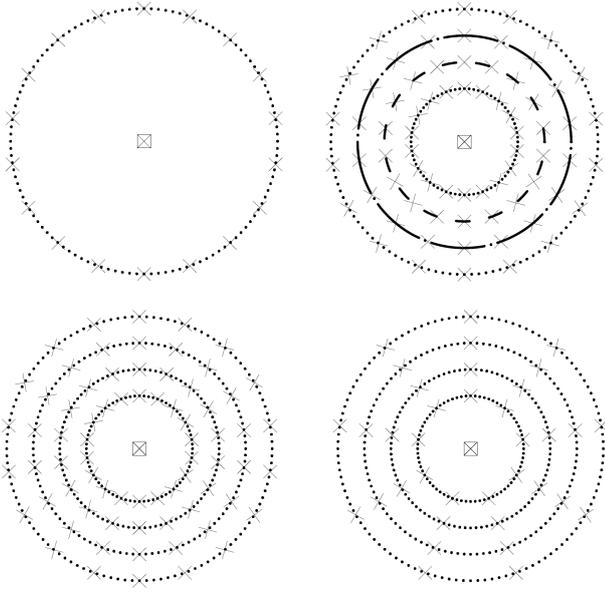


FIGURE 2. The different strategies for selection of sampling points. The boxed cross represents boundary condition application (zero velocity) in case of fixed particle, the open cross indicate location of sampling point.

Find $\mathbf{u}_h^{n+2/3} \in \mathbb{W}_h$ such that

$$\begin{aligned} \varrho \int_{\Omega} \frac{\mathbf{u}_h^{n+2/3} - \mathbf{u}_h^{n+1/3}}{\Delta t} \cdot \mathbf{v}_h \, d\mathbf{x} \\ - \varrho \int_{\Omega} (\mathbf{u}_h^{n+1/3} \cdot \nabla) \mathbf{u}_h^{n+2/3} \cdot \mathbf{v}_h \, d\mathbf{x} \\ + 2\alpha\eta \int_{\Omega} \mathbf{D}[\mathbf{u}_h^{n+2/3}] : \mathbf{D}[\mathbf{v}_h] \, d\mathbf{x} = 0 \end{aligned} \quad \text{for all } \mathbf{v}_h \in \mathbb{V}_h. \quad (17)$$

Finally find $\mathbf{u}_h^{n+1} \in \mathbb{W}_h$, $\boldsymbol{\lambda}_h^{n+1} \in \Lambda_h$ such that

$$\begin{aligned} \varrho \int_{\Omega} \frac{\mathbf{u}_h^{n+1} - \mathbf{u}_h^{n+2/3}}{\Delta t} \cdot \mathbf{v}_h \, d\mathbf{x} \\ + 2\beta\eta \int_{\Omega} \mathbf{D}[\mathbf{u}_h^{n+1}] : \mathbf{D}[\mathbf{v}_h] \, d\mathbf{x} = \langle \boldsymbol{\lambda}_h^{n+1}, \mathbf{v}_h \rangle \end{aligned} \quad \text{for all } \mathbf{v}_h \in \mathbb{V}_h, \quad (18)$$

$$\langle \boldsymbol{\mu}_h, \mathbf{u}_h^{n+1} \rangle_P = 0 \quad \text{for all } \boldsymbol{\mu}_h \in \Lambda_h. \quad (19)$$

This scheme is only first order accurate, but with good stability properties, see [5]. The described method has also been used in [6].

4. SAMPLING POINT SELECTION

As already mentioned, the rigid body or no flow constraints are imposed in a weak sense using Lagrange multipliers. In a practical implementation, the corresponding integral in a weak form is evaluated as a sum over a set of discrete sampling points. In this paper, we have proposed and tested several strategies to enforce constraints by combining one or more Lagrange multipliers per particle and using different strategies for the sampling point selection. For the considered

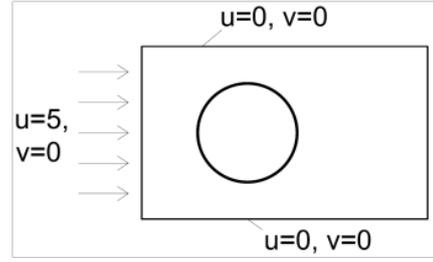


FIGURE 3. The problem of 2D flow around single obstacle.

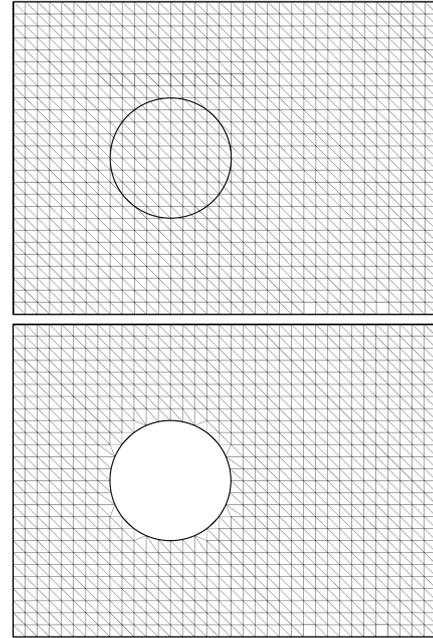


FIGURE 4. The mesh of 2D flow with single obstacle.

circular geometry of particle, the proposed strategies consist of generating the different patterns of sampling points in radial and longitudinal directions, see Figure 2. These results of these strategies are compared using two test scenarios to results obtained with fully resolved simulations, where the geometry of each individual particle is represented exactly by the mesh and corresponding no-flow constraints are exactly satisfied.

5. NUMERICAL TESTS

5.1. FLOW AROUND SINGLE OBSTACLE

The first example to evaluate proposed strategies solves the 2D flow around a single, rigid particle. The geometry of the problem is depicted in Figure 3, together with initial and boundary conditions. The perfect friction (no slip) boundary condition has been assumed on horizontal edges. The domain has been discretized into 1820 triangular Taylor-Hood elements, see Figure 4 top. The values of mass density $\varrho = 1.0 \text{ kg/m}^3$, viscosity $\eta = 10^{-1} \text{ Pa}\cdot\text{s}$, and time step $\Delta t = 0.001 \text{ s}$ have been used in this study.

The described model has been implemented into

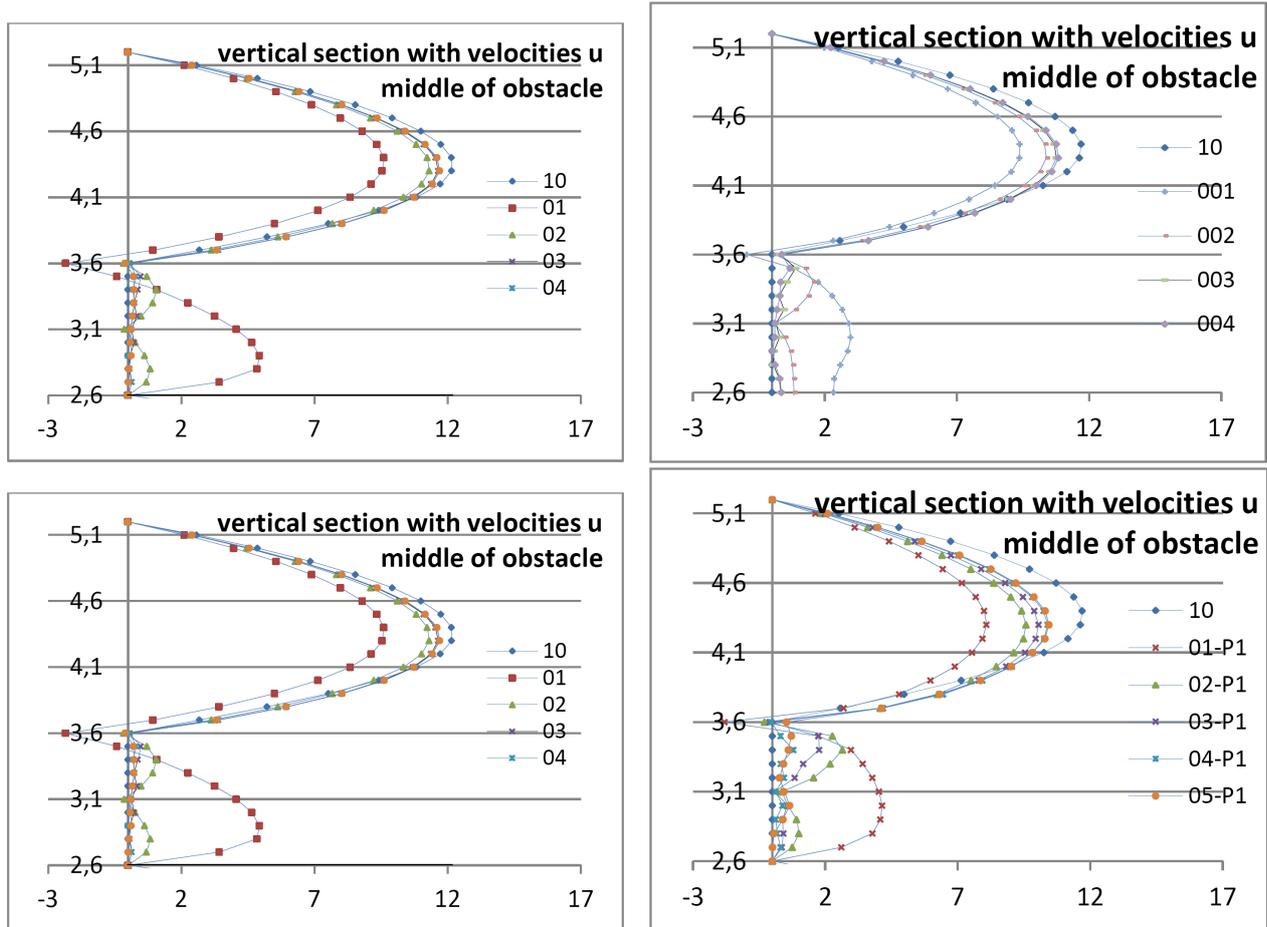


FIGURE 5. Velocity profiles through obstacle.

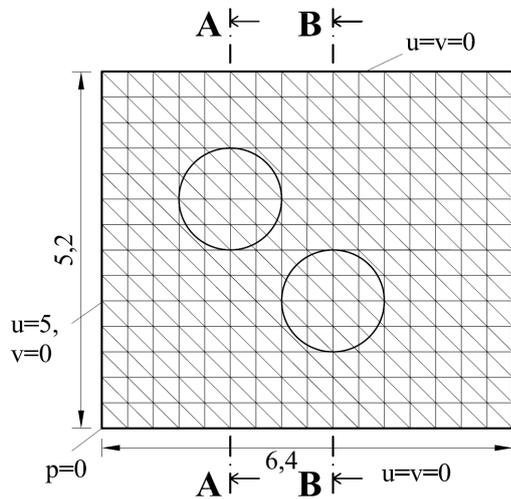


FIGURE 6. The geometry and the boundary conditions of the flow in tube with obstacle (448 el.).

an object oriented FE code oofem [13]. The different strategies for a selection of sampling points have been evaluated and compared to results obtained by fully resolved simulation (see Figure 4 bottom for discretization, consisting of 1656 elements and 3462 nodes). The comparison with fully resolved simulation has been made at a steady state.

The individual strategies considered are described in Table 1. The Figure 5 shows the profiles of velocity (horizontal component) in a vertical section passing through the particle center. Table 1 also contains the L2 norm of the difference of the obtained velocity and velocity from fully resolved simulation along the vertical profile passing the center of the particle. The obtained results indicate that an optimum strategy for sampling point selection is to have multiple rings with a dedicated multiplier for each ring. The best result (in terms of smaller difference) has been obtained for strategy 05 consisting of 12 rings and 12 multipliers for each ring. However, it is necessary to balance the computational effort (related to number of rings and number of multipliers) and obtained error. From this point of view, the optimal seems to be the strategy 03 with 4 rings.

5.2. FLOW AROUND TWO OBSTACLES

The second example represents a flow in a tube with two particles, as illustrated in Figure 6. In this test, three different discretizations of the fictitious domain have been used with an increasing mesh density, containing 448, 1792, and 7168 elements. The perfect friction on both horizontal edges (no slip condition) has been assumed. The results are again compared by means of comparing the velocity profiles along the

No.	Lagrange multipliers	Figure	Error L^2 -norm
10	fully resolved simulation		0
01	1 multiplier per ring – 1 ring	15 A	58.10
02	1 multiplier per ring – 2 rings	15 B	9.36
03	1 multiplier per ring – 4 rings	15 B	1.13
04	1 multiplier per ring – 8 rings	15 B	0.93
05	1 multiplier per ring – 12 rings	15 B	0.89
001	1 multiplier for 2 rings	15 C	22.66
002	1 multiplier for 4 rings	15 C	7.48
003	1 multiplier for 8 rings	15 C	4.45
004	1 multiplier for 12 rings	15 C	4.04
01-P1	same as 01 – sporadic points	15 D	56.33
02-P1	same as 02 – sporadic points	15 D	21.10
03-P1	same as 03 – sporadic points	15 D	13.92
04-P1	same as 04 – sporadic points	15 D	9.76
05-P1	same as 05 – sporadic points	15 D	8.88

TABLE 1. Different ways of introducing of sample points with L^2 norm of velocity difference in vertical profile passing the center of obstacle.

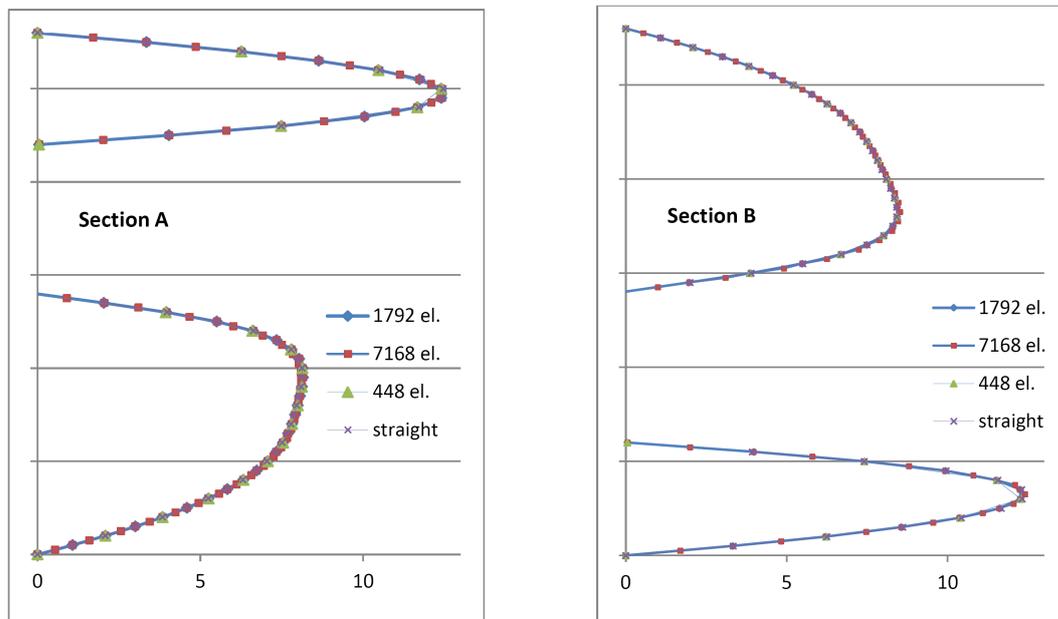


FIGURE 7. Vertical profiles of velocity passing the centers of both particles.

vertical section, indicated in Figure 6. Four (eight, twenty-four) Lagrange multipliers per obstacle have been used. Figure 6 shows obtained velocity profiles using the fictitious domain method and using the fully resolved simulation.

The obtained results show excellent agreement to the results obtained by the fully resolved simulation.

6. CONCLUSION

The presented paper deals with the modelling of incompressible flow around fixed (or moving, rigid) particles using the concept of fictitious domain method and demonstrates the capability of this method to describe the flow with solid obstacles.

The paper demonstrates that the accuracy of the method depends on the strategy of choosing sampling points in addition to traditional aspects, such as time stepping and integration or space discretization. From the simulations performed using different strategies, the uniform distribution of sampling points is strongly recommended, while each element should contain at least 1 sampling point. Although the obtained results are problem and grid dependent, they demonstrate the clear dependence of the sampling point selection on the quality of the solution.

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